

Impact of Various Ply Orientations on the Buckling Load of Laminated Composites

Lohitha S J¹, Shruthi N P², Manju N L³

¹Lecturer, Department of Civil Engineering, DRR Government Polytechnic Davangere, Karnataka, India.

²Lecturer, Department of Civil Engineering, Government Polytechnic Harihara, Karnataka, India.

³Lecturer, Department of Civil Engineering, Government Polytechnic Siddapura, Karnataka, India.

ABSTRACT:

Composite plates that are laminated are made up of layers of bonded materials that have different chemical compositions and are combined together in a macroscopical manner. Plates made of laminated composite material that have holes in them are less stiff, less resistant to inertia, and weaker than plates that do not have holes. The optimization and nonlinear behavior of square and cylindrical laminated plates with and without cuts, as well as their behavior without cuts under buckling stresses, are the subjects of this research. Cutouts are necessary for a number of reasons, including ventilation, cable attachments, and weight reduction, and they are essential in order to get the desired result of reducing weight. As part of the evaluation process, specifics like the location of the cutout, the angle at which the fibers are oriented, the proportion of length to thickness, the boundary condition, and the Young's Modulus Ratio are being considered. The laminated plates that were investigated were made of carbon fiber reinforced composites, which are the sorts of materials investigated. When compared to plates that do not have the cutouts, laminated composite plates that have circular cutouts have a lower buckling load.

Keywords: Buckling Analysis, Finite Element Method, Laminated Composite Plate, Ply Orientation.

I. INTRODUCTION

Buckling is a property that composite laminated plates exhibit when they are subjected to compression. Composites are made up of two or more materials that, when mixed, combine to provide qualities that would have been difficult to achieve with just one of those components alone. The majority of the weight that is carried by these kinds of materials is carried by the fibers. Matrixes that have a low modulus and a high elongation enable structures to function in a flexible manner while also shielding fibers from the pressures of the environment and ensuring that they remain in their proper position. Composite materials, which are made up of two or more components, provide a significant decrease in the weight of the structure while yet retaining a high level of strength via their composition. When it comes to building, fiber-reinforced composites often take the form of a lamina, which is a thin layer. Laminae are the most common kind of material macrounit. It is possible to modify the stacking sequence of the layers and the orientation of the fibers in each lamina in order to get the required level of strength and stiffness for a specific job. It is the unique combination of attributes that are brought about by the composition, distribution, and orientation of the components that make up a composite that is responsible for the material's properties. There are a number of reasons why cutouts are necessary, including but not limited to the reduction of weight, the facilitation of air circulation, and the establishment of connections with other units. Carbon-fiber reinforced plastic is a composite material that is created by combining a number of different kinds of carbon fibers with thermosetting resins. A material that is extraordinarily durable, carbon fiber reinforced plastic (CFRP) is lightweight, nonconductive, and reinforced with fibers. It is also feasible to boost the material's strength and stiffness attributes in an effective manner by stacking a large number of fiber layers with a variety of desired orientations. The finite element method was used by Parth Bhavsar and colleagues in order to investigate the buckling behavior of glass fiber reinforced polymer (GFRP) when it was subjected to linearly varying loading.

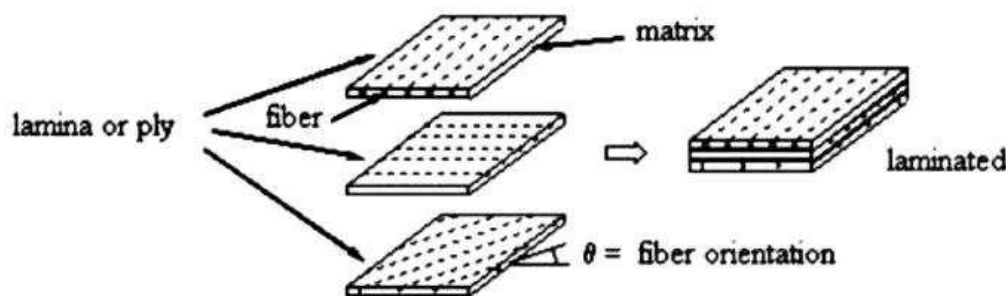


Figure 1: Laminated Composite Plate

Several parameters have been investigated by researchers in order to determine how they influence the buckling stress of rectangular plates with aspect ratios of 1. The two-dimensional finite element analysis was used by Joshi et al. in order to determine the buckling load per unit length in a rectangular plate that had circular cut-outs and was subjected to bi-axial compression. One is able to evaluate the buckling factors by adjusting the length-to-thickness ratio as well as the positioning of the holes. Nagendra Singh Gaira and colleagues investigated the buckling response of laminated rectangular plates that were subjected to clamped-free boundary conditions. It should be noted that the presence of cut-out results in a reduction in the buckling load. As the aspect ratio rises, the buckling load factor decreases, which is the desired result. Using a laminated composite cylindrical panel with an elliptical cut-out of varied sizes and locations, Hamidreza Allahbakhsh and Ali Dadrasi carried out a buckling analysis in order to investigate the impact that an axial load has on the buckling load of the panel. Bucket Okutan Baba studies the ways in which the buckling stress on rectangular plates is affected by a variety of cut-out geometries, length/thickness ratios, and ply orientations.

The researchers used both computational and experimental methodologies in order to make their determinations about the effects of these hits on the buckling behavior of E-glass/epoxy composite plates that were exposed to an in-plane compression stress. In their finite element buckling analysis of composite laminate skew plates that were subjected to uniaxial compressive loads, Hsuan-Teh Hu and colleagues discovered that, in comparison to the linearized buckling loads of the skew plates, the failure criterion and nonlinear in-plane shear have a significant impact on the ultimate loads of the composite laminate skew plates.

1. Numerical Analysis Using Finite Element Method and Material

An technique that is straightforward in order to fulfill the criteria of the conference paper format in order to accomplish the objective of this research, the buckling load factors of square and cylindrical carbon fiber composite plates will be determined using the use of finite element analysis. The APDL version is ANSYS 14.5. $L \times t$ are the dimensions of the plate when it is subjected to three separate boundary conditions: fixed, clamped, and unclamped circumstances. There are two layers in the first scenario, while there are three levels in the second scenario. This is due to the fact that the stacking sequence that is used is $[0^0/90^0]$ and $[0^0/90^0/0^0]$ respectively. In order to carry out the research, the plate is punched with a number of center holes that are of the same volume. It is possible for the central holes to be fashioned in a round, square, triangle, or star pattern. There is an investigation into the nature of the buckling load factor.

2. Element Description

Within the scope of this inquiry, the SHELL281 element type is being used. Researching shells that are either very thin or relatively thick may be accomplished with the use of this shell element. Additionally, because to its layered applications, it is excellent for simulating sandwich structures as well as laminated composite coatings. Applications that involve high strain nonlinearity, linearity, or rotation are perfect for their use of this material. Six degrees of freedom are available at each of the eight nodes that make up the element. These degrees of freedom enable rotation around the three axes as well as translations along the axes of x , y , and z inside the element. Studies involving cylindrical plates make use of the nonlinear element S8R5, which consists of eight nodes and has five degrees of freedom for each node involved.

3. Geometric Modelling

The length of square plates may be any length beginning at 500 millimeters. It is assumed that the diameter of the hole in the middle is fifty millimeters. In the case of cylindrical specimens, nominations might vary anywhere from L500 to R200. The number that comes after the letter L denotes the length of the panel, and the number that comes after the letter R denotes the radius of the panel. The plate is offered in four distinct thicknesses, which are as follows: 2 millimeters, 2.5 millimeters, 3 millimeters, and 3.5 millimeters.

Table 1: Properties of carbon material

Young's modulus (Pa)	$E_{11}=1.397 \times 10^{11}$	$E_{33}=1.139 \times 10^{11}$
Poisson's ratio	$\nu_{12}=0.3236$	$\nu_{13}=0.3236$
Rigidity modulus (Pa)	$G_{12}=4.753 \times 10^9$	$G_{13}=4.753 \times 10^9$

4. Model of Carbon Composite Plate

The length of square plates may be any length beginning at 500 millimeters. It is assumed that the diameter of the hole in the middle is fifty millimeters. In the case of cylindrical specimens, nominations might vary anywhere from L500 to R200. The number that comes after the letter L denotes the length of the panel, and the number that comes after the letter R denotes the radius of the panel.

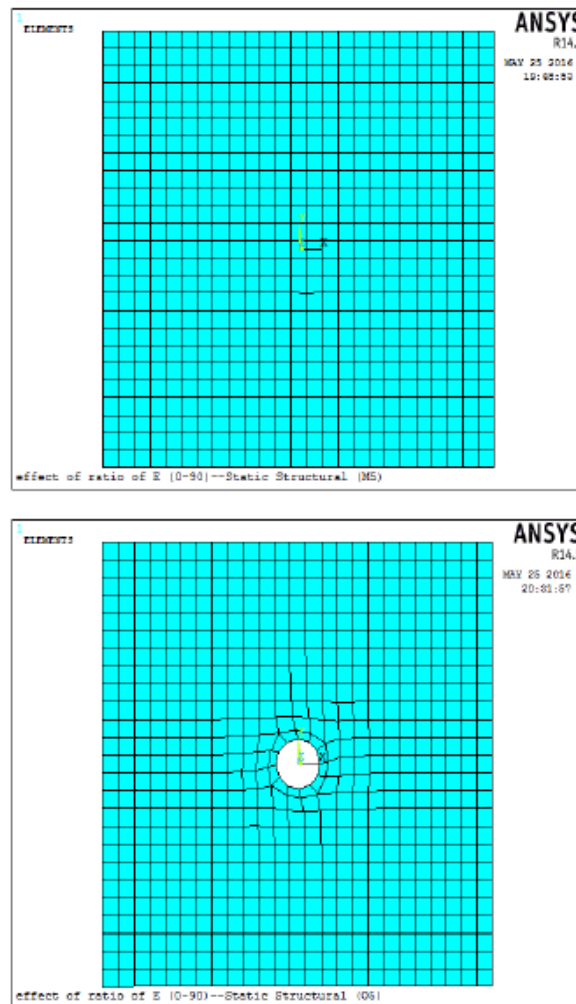


Figure 2 : Model of square plate without and with cut-out

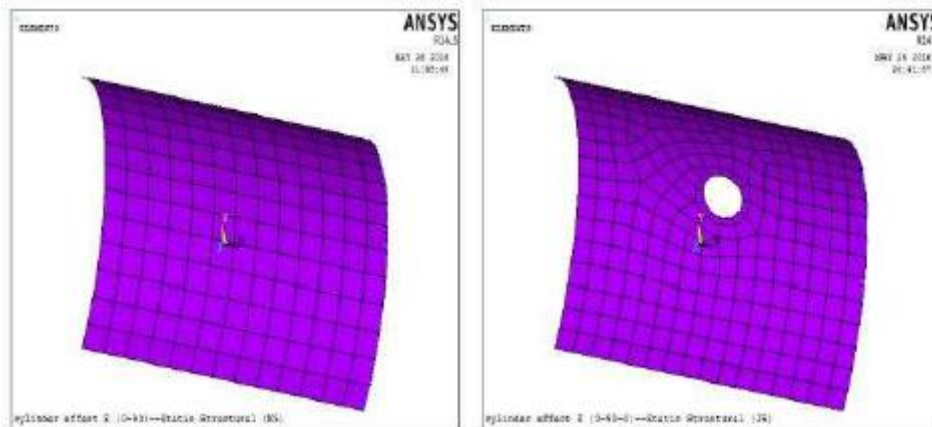


Figure 3: Model of cylindrical plate without and with cut-out

II. RESULTS AND DISCUSSION

When the plate is exposed to the same boundary condition, the objective of this section is to study the influence that different ply orientations of the plate have on the plate. This particular circumstance is a fixed border condition, and it is being taken into consideration. The following is a list of the several ply orientations that are used in this section: (0/0/0), (0/30/0), (0/45/0), (0/90/0), (90/90/90), and (90/0/90).

Analysis is performed on both of them, and an investigation into the consequences of it is carried out.

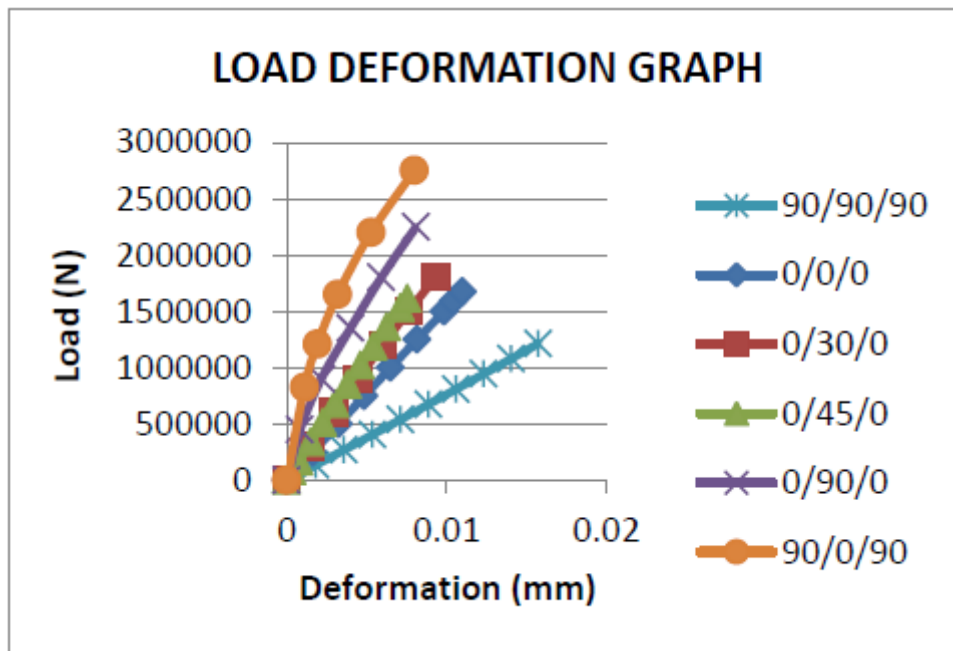


Figure 4 : Buckling load deformation graph of plates with ply orientations

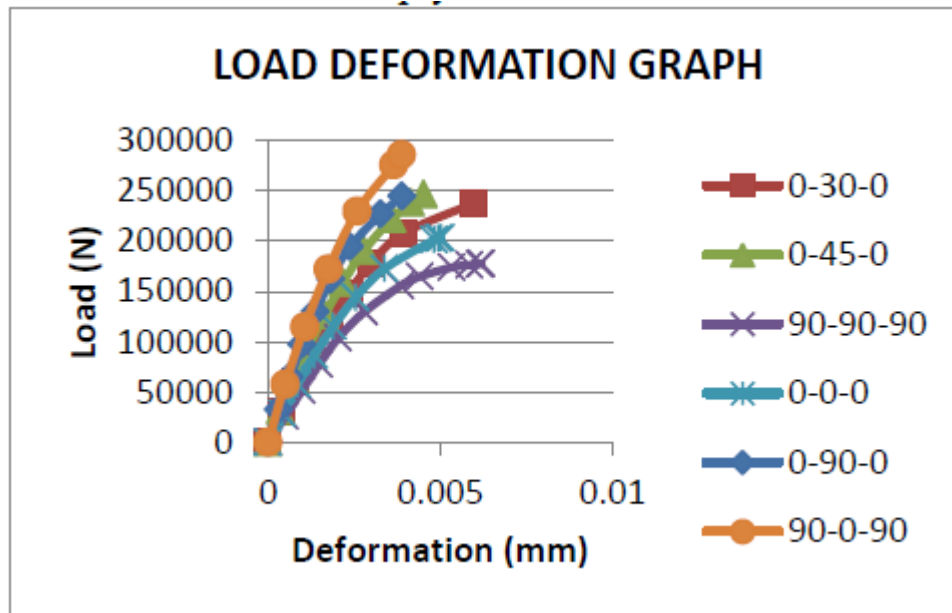


Figure 5 : Buckling load deformation graph of cylindrical plates with ply orientations

Given that it is commonly acknowledged that the greatest load bearing capacity is for the fixed boundary condition, the fixed condition is being used here as the border. This is because the fixed condition constitutes the boundary. These requirements are applied to laminated plates that are either square or cylindrical, and they are considered to be within the scope of this section. Figures 4 and 5 illustrate the load deformation graph of plates that have ply orientations that are different from one another. With the assistance of this graph, we are able to get a solid understanding of the buckling effect that occurs when plates are subjected to loads. In contrast to the other ply angles, the buckling load that is shown by the (90/0/90) ply angle is the one that makes the most significant contribution. When it comes to the buckling load bearing ply orientation, the value that is considered to be the lowest feasible is (90/90/90). In particular, we focused our investigation on a laminated composite plate that had a circular cut-out in the middle of the plate. This is because our study, which was reported in the part before this one, demonstrates that a square laminated composite plate with a central circular cut-out has a positive buckling load effect under cut-out plates. This is the reason why this is the case.

III. CONCLUSIONS

An examination of the buckling response of laminated composite plates with various ply orientations conditions is being carried out as part of this investigation.

At the same time, it is essential to take into account the fact that the laminated composite plates have a range of aspect ratios, changing width to thickness ratios, cut out forms, and variable positions for holes. There are a great number of conclusions that may be derived from the present research, some of which are as follows: The buckling load increases as the ratio of the L to the t decreases. A decrease in the buckling load is brought about as a consequence of the existence of cut-out. When there is a cut-out present, the surface area decreases, which leads to a reduction in the load that is required to buckle the plate and cause it to distort its form. This is because the plate is forced to buckle under the strain. The buckling load is thus reduced as a consequence of this. As the number of layers increases, the buckling load begins to increase in a manner that is proportional to the number of layers. As the number of layers grows, the interaction between each layer likewise increases. This is the reason why this is the case. As a consequence of this, a considerable amount of load is required in order to accomplish the critical buckling load. When the EL/ET ratio is increased, the buckling load also increases in proportion to the size of the increase. It is possible for the amount of weight that is buckling to change according on the cut-out shapes that are used. When it comes to circular cut-outs, the buckling load is discovered to be the greatest amount that is even remotely achievable. The buckling load is also the lowest feasible value for star cuts of the same size. This is an additional point to consider.

REFERENCES

- [1]. Thai H-T, Kim S-E. Free vibration of laminated composite plates using two variable refined plate theory. *Int J Mech Sci* 2010; 52:626–33.
- [2]. Ngo-Cong D, Mai-Duy N, Karunasena W, Tran-Cong T. Free vibration analysis of laminated composite plates based on FSDT using one-dimensional IRBFN method. *Comput Struct* 2011; 89:1–13.

- [3]. Xiang S, Jiang S, Bi Z, Jin Y, Yang M. A nth-order mesh less generalization of Reddy's third-order shear deformation theory for the free vibration on laminated composite plates. *Compos Struct* 2011; 93:299–307.
- [4]. Motley MR, Kramer MR, Young YL. Free surface and solid boundary effects on the free vibration of cantilevered composite plates. *Compos Struct* 2013; 96:365–75.
- [5]. Ahmed JK, Agarwal VC, Pal P, Srivastav V. Static and dynamic analysis of composite laminated plate. *Int J Innov Technol Explor Eng* 2013; 3:56–60.
- [6]. Sharma AK, Mittal ND. Free vibration analysis of laminated composite plates with elastically restrained edges using FEM. *Cent Eur J Eng* 2013; 3:306–15.
- [7]. Malekzadeh P, Zarei AR. Free vibration of quadrilateral laminated plates with carbon nanotube reinforced composite layers. *Thin-Walled Struct* 2014; 82:221–32.
- [8]. Thinh TI, Nguyen MC, Ninh DG. Dynamic stiffness formulation for vibration analysis of thick composite plates resting on non-homogenous foundations. *Compos Struct* 2014; 108:684–95.
- [9]. Boscolo M, Banerjee JR. Layer-wise dynamic stiffness solution for free vibration analysis of laminated composite plates. *J Sound Vib* 2014; 333:200–27.
- [10]. Sayyad AS, Ghugal YM. On the free vibration analysis of laminated composite and sandwich plates: A review of recent literature with some numerical results. *Compos Struct* 2015; 129:177–201.
- [11]. Mantari JL, Ore M. Free vibration of single and sandwich laminated composite plates by using a simplified FSDT. *Compos Struct* 2015; 132:952–9.
- [12]. Belarbi M-O, Tati A, Ounis H, Khechai A. On the Free Vibration Analysis of Laminated Composite and Sandwich Plates: A Layerwise Finite Element Formulation. *Lat Am J Solids Struct* 2017; 14:2265–90.
- [13]. Pingulkar P, Suresha B. Free vibration analysis of laminated composite plates using finite element method. *Polym Compos* 2016; 24:529–38.
- [14]. Mahabadi RK, Shakeri M, Pazhooh MD. Free vibration of laminated composite plate with shape memory alloy fibers. *Lat Am J Solids Struct* 2016; 13:314–30.
- [15]. Phan-Dao H-H. A meshfree radial point interpolation method for free vibration of laminated composite plates analysis based on layerwise theory. *Procedia Eng* 2016;142:349–56.