



## A Modified Homotopy Perturbation Method for Efficient Analysis of Nonlinear Rotating Pendulum Dynamics

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### **Abstract:**

*This paper presents a development and enhancement of the Modified Homotopy Perturbation Method (MHPM) for solving strongly nonlinear oscillatory problems, with application to the rotating pendulum model. The method allows for obtaining highly accurate approximate solutions for frequency and time response without the need to expand trigonometric functions like sine into Taylor series, thereby preserving accuracy even at large deflection angles. The results are compared with other established methods such as the Homotopy Analysis Method (HAM), Gamma Function Method (GFM), and Harmonic Balance Method (HBM). MHPM demonstrates clear superiority in terms of accuracy and relative error, especially at large amplitudes and high rotational speeds. The study provides a detailed analysis of the influence of rotational speed ( $\Lambda$ ) and amplitude ( $A$ ) on the system's dynamics and confirms the method's efficiency in modeling complex nonlinear systems.*

### **Keywords:**

*Modified Homotopy Perturbation Method, rotating pendulum, nonlinear vibrations, approximate frequency, comparative analysis, nonlinear dynamical systems.*

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### **I. Introduction**

Many engineering problems can be modeled by nonlinear ordinary or partial differential equations, but obtaining exact solutions is often highly complex or even impossible, with only a few exceptions. This complexity arises from the intrinsic nature of nonlinearity, where interactions between variables are not directly proportional, leading to behaviors such as bifurcations, chaos, and other intricate dynamics. As a result, asymptotic solutions, which approximate solutions under specific limiting conditions, have gained significant attention among scientists and engineers tackling various nonlinear equations.

For weakly nonlinear problems, classical methods like the averaging method and the small parameter method have been commonly employed. These techniques simplify the original problem into a form that can be more easily analyzed, often by isolating dominant terms and treating others as perturbations. In addition to these foundational approaches, more advanced methods such as the multiple scales (MS) method and the Lindstedt–Poincaré (LP) method have been developed. These methods offer valuable advantages in solving vibratory systems by addressing resonance and periodic solutions in nonlinear dynamics. However, their accuracy critically depends on the proper selection of a small parameter, and an incorrect choice may lead to erroneous or physically unrealistic solutions.[1]

## II. Modified homotopy perturbation method

For describing the method at first, we take into account an oscillator with strong nonlinearity as [2]

$$\ddot{u} + \omega_0^2 u + f(u, \dot{u}, \ddot{u}) = 0, \quad (1)$$

$$\ddot{u} + \omega_0^2 u + f(u, \dot{u}, \ddot{u}) = 0,$$

where the dots over the variable  $u$  represent derivative with respect to time,  $t$ , unperturbed frequency of the oscillator is  $\omega_0$  and the nonlinear function is represented by  $f(u, \dot{u}, \ddot{u})$ . The initial conditions of the oscillator are given as

$$u(0) = A, \dot{u}(0) = 0. \quad (2)$$

If we chose  $\tau = \omega t$ , equation (1) is transformed to

$$\omega^2 u'' + \omega_0^2 u + f(u, \omega u', \omega^2 u'') = 0, \quad (3)$$

where primes on  $u$  represent derivative with respect to  $\tau$  and the initial conditions are transformed as  $u(0) = A$ ,  $u'(0) = 0$ . We consider the homotopy for the equation (3) as

$$\omega^2 u' + \omega^2 u + p(-\omega^2 u + \omega_0^2 u + f(u, \omega u', \omega^2 u'')) = 0. \quad (4)$$

According to the present MHPM, solution of the equation (4) is considered as

$$u = u_0 + pu_1 + p^2 u_2 + p^3 u_3 + \dots, \quad (5)$$

while the frequency response is considered as

$$\omega^2 = \omega_0^2 (1 + p\omega_1 + p^2\omega_2 + p^3\omega_3 + \dots). \quad (6)$$

We now use the values of  $u$  and  $\omega^2$  from equations (5) and (6) into equation (4) and expand the resulting equation in a power series of  $p$  and then equate the coefficient of various powers of  $p$  from both sides to get a set of linear differential equations. These equations are solved in sequence to determine the solution and frequency response.[2]

We can see from equation (4), as  $p \rightarrow 1$ , it reduces to equation (1), whereas equations (5) and (6) are written as

$$u = u_0 + u_1 + u_2 + u_3 + \dots, \quad (7)$$

and

$$\omega^2 = \omega_0^2 (1 + \omega_1 + \omega_2 + \omega_3 + \dots). \quad (8)$$

The MHPM solution and frequency response of equation (1) is thus represented by equations (7) and (8).

## III. Examples

**The rotating pendulum (3.1)[3]** The subsequent implementation, as illustrated in Figure 3.1, utilizes nonlinear differential equations (NLDEs) to thoroughly simulate the dynamic behavior of a simple pendulum attached to a rotating solid framework. By integrating NLDEs, the model offers a more precise and realistic depiction of the pendulum's response to rotational influences. The system's governing equation of motion is

$$\ddot{u} + (1 - \Lambda \cos u) \sin u = 0, \quad (9)$$

where  $\Lambda = \frac{\Omega^2 r}{g}$  and the initial conditions are specified as  $u(0) = A$ ,  $\dot{u}(0) = 0$ .

If  $\omega$  represents the frequency of the oscillator, equation (9) can be expressed as

$$\omega^2 u'' + (1 - \Lambda \cos u) \sin u = 0, \quad (10)$$

where  $\tau = \omega t$ ,  $u' = \frac{du}{dt}$  and the initial conditions are converted to  $u(0) = A$ ,

$u'(0) = 0$ : According to the present method the homotopy for equation (10) is considered as

$$\omega^2 u'' + \omega^2 u (-\omega^2 u + \sin u - \Lambda \cos x \sin x) = 0, \quad (11)$$

Substituting the values of  $u$  and  $\omega^2$  from equations (5) and (6) into equation (11) and equating the terms from both sides with the same powers of  $p$ , we can derive a series of linear differential equations, of which we present only the first three as

$$\omega_0^2 u_0'' + \omega_0^2 u_0 = 0; u_0(0) = A, u_0'(0) = 0 \quad (12)$$

$$\omega_0^2 u_1'' + \omega_0^2 u_1 = u_0 \omega_0^2 - \sin u_0 + \Lambda \cos u_0 \sin u_0 - u_0 \omega_0^2 \omega_1 - u_0'' \omega_0^2 \omega_1; u_1(0) = 0, u_1'(0) = 0 \quad (13)$$

$$\begin{aligned} \omega_0^2 u_2'' + \omega_0^2 u_2 &= u_1 \omega_0^2 - u_1 \cos u_0 + \Lambda u_1 \cos^2 u_0 - \Lambda u_1 \sin^2 u_0 + u_0 \omega_0^2 \omega_1 - u_1 \omega_0^2 \omega_1 \\ &\quad - u_1'' \omega_0^2 \omega_1 - u_0 \omega_0^2 \omega_2 - u_0'' \omega_0^2 \omega_2; u_1(0) = 0, u_1'(0) = 0 \end{aligned} \quad (14)$$

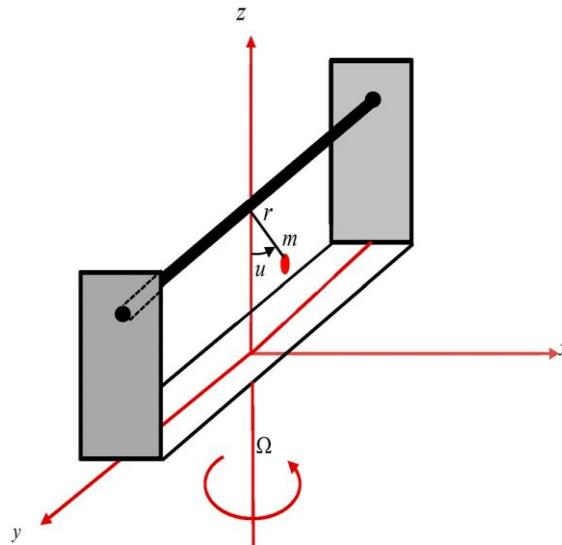


Figure 3.1. Schematic of a rotating pendulum.

The solution of equation (12) is

$$u_0 = A \cos \tau \quad (15)$$

By substituting the value of  $u_0$  into equation (13) and simplifying, we obtain

$$\begin{aligned} \omega_0^2 u_1'' + \omega_0^2 u_1 &= \omega_0^2 A \cos \tau - \sin(A \cos \tau) + \Lambda \sin(A \cos \tau) \cos(A \cos \tau) = \omega_0^2 A \cos \tau - \sin(A \cos \tau) + \frac{\Lambda}{2} \sin(2A \cos \tau) \\ (16) \end{aligned}$$

Fourier series expansions for  $\sin(A \cos \tau)$  and  $\sin(2A \cos \tau)$  are considered as

$$\sin(A \cos \tau) = \sum_{n=0}^{\infty} l_{2n+1} \cos[(2n+1)\tau] = l_1 \cos \tau + l_3 \cos 3\tau + \dots, \quad (17)$$

where

$$\text{and } l_{2n+1} = \frac{4}{\pi} \int_0^{\pi/2} \sin(A \cos \tau) \cos[(2n+1)\tau] d\tau = 2(-1)^n J_{2n+1}(A), \quad (18)$$

$$\sin(2A \cos \tau) = \sum_{n=0}^{\infty} e_{2n+1} \cos[(2n+1)\tau] = e_1 \cos \tau + e_3 \cos 3\tau + \dots, \quad (19)$$

where

$$e_{2n+1} = \frac{4}{\pi} \int_0^{\pi/2} \sin(2A \cos \tau) \cos[(2n+1)\tau] d\tau = 2(-1)^n J_{2n+1}(2A). \quad (20)$$

We consider  $I_{2n+1}(A)$  as the Bessel function of the first kind of  $(2n+1)$ -order. The first term for both these series is obtained as  $l_1 = 2J_1(A)$  and  $e_1 = 2J_1(2A)$ . Where  $J_1(A)$  is the first-order Bessel function of the first kind. Substitution of these results into equation (16) gives

$$\omega_0^2 u_1'' + \omega_0^2 u_1 = \omega_0^2 A \cos \tau - 2J_1(A) \cos \tau + AJ_1(2A) \cos \tau - \sum_{n=1}^{\infty} l_{2n+1} \cos[(2n+1)\tau] + \frac{k}{2} \sum_{n=1}^{\infty} e_{2n+1} \cos[(2n+1)\tau]. \quad (21)$$

Avoiding secular term, we get

$$\omega_0^2 = \frac{2J_1(A) - AJ_1(2A)}{A}. \quad (22)$$

Thus, the zeroth-order approximate frequency is

$$\omega_0 = \sqrt{\frac{2J_1(A) - AJ_1(2A)}{A}}. \quad (23)$$

Which is same as the first-order approximate frequency determined by Moatimid et al. Remaining part of equation (21) is written as follows:

$$\omega_0^2 u_1'' + \omega_0^2 u_1 = \frac{A}{2} \sum_{n=1}^{\infty} e_{2n+1} \cos[(2n+1)\tau] - \sum_{n=1}^{\infty} l_{2n+1} \cos[(2n+1)\tau], \quad (24)$$

with initial conditions  $u_1(0) = 0$ ,  $u_1'(0) = 0$ . The solution to equation (24) is chosen as follows:

$$u_1 = \sum_{n=0}^{\infty} b_{2n+1} \cos[(2n+1)\tau]. \quad (25)$$

Substituting equations (4.2.25) into (4.2.24) gives

$$-\omega_0^2 \sum_{n=1}^{\infty} 4n(n+1) b_{2n+1} \cos[(2n+1)\tau] = \frac{A}{2} \sum_{n=1}^{\infty} e_{2n+1} \cos[(2n+1)\tau] - \sum_{n=1}^{\infty} l_{2n+1} \cos[(2n+1)\tau], \quad (26)$$

and then we can write the following expression for the coefficients  $b_{2n+1}$ :

$$b_{2n+1} = \frac{l_{2n+1}}{4n(n+1)\omega_0^2} - \frac{\Lambda e_{2n+1}}{8n(n+1)\omega_0^2} = \frac{2(-1)^2 J_{2n+1}(A)}{4n(n+1)\omega_0^2} - \frac{\Lambda(-1)^2 J_{2n+1}(2A)}{4n(n+1)\omega_0^2}, \quad (2)$$

7)

for  $n \geq 1$ . Considering that  $u_1(0) = 0$ , equation (25) gives

$$b_1 = - \sum_{n=1}^{\infty} b_{2n+1}. \quad (28)$$

From equation (14), it is obvious that the value of  $u_1$  is required to determine the higher-order approximate solution  $u_2$ . But  $u_1$  has infinite number of terms, which will create difficulties to obtain the higher-order solution  $u_2$ . However, we can truncate the series expansion of  $u_1$  presented in equation (25) and express an approximate equation  $u_1^{(N)}$  in the form

$$\text{and } b_1^{(N)} = - \sum_{n=1}^N b_{2n+1}, \quad (29)$$

$$u_1^{(N)} = \sum_{n=0}^N b_{2n+1} \cos[(2n+1)\tau], \quad (30)$$

which contains only a finite number of harmonics. By comparing equations (25) and (29), we find that

$$\lim_{N \rightarrow \infty} u_1^{(N)} = u_1, \quad (31)$$

$$\lim_{N \rightarrow \infty} b_1^{(N)} = b_1. \quad (32)$$

For simplicity, we can consider  $N = 2$  in equation (4.2.29) and we obtain

$$u_1^{(2)} = b_1^{(2)} \cos \tau + b_3 \cos 3\tau = b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau), \quad (33)$$

$$b_3 = \frac{l_3}{8\omega_0^2} - \frac{\Lambda e_3}{16\omega_0^2}, \quad (34)$$

$$b_5 = \frac{l_5}{24\omega_0^2} - \frac{\Lambda e_5}{48\omega_0^2},$$

where  $l_3, l_5, e_3$  and  $e_5$  are given. Thus, the first-order approximate solution is

$$u_1^{(2)} = b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau). \quad (35)$$

The first approximate frequency  $\omega_1$  can be derived by applying the no secular term condition on equation (14).

Now substituting the value of  $u_0$  and  $u_1^{(2)}$ , equation (14) becomes

$$\begin{aligned}
& \omega_0^2 u_2'' + \omega_0^2 u_2 = \omega_0^2 (b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau)) \\
& - (b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau)) \cos(A \cos \tau) + A(b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau)) \\
& - \cos(2A \cos \tau) + \omega_0^2 \omega_1 A \cos \tau - \omega_0^2 \omega_1 (b_3(\cos 3\tau - \cos \tau) + b_5(\cos 5\tau - \cos \tau)) \\
& + \omega_0^2 \omega_1 (b_3(9 \cos 3\tau - \cos \tau) + b_5(25 \cos 5\tau - \cos \tau)).
\end{aligned} \tag{36}$$

It is possible to do the following Fourier series expansion

$$(\cos 3\tau - \cos \tau) \cos(A \cos \tau) = \sum_{n=0}^{\infty} m_{2n+1} \cos[(2n+1)\tau] = m_1 \cos \tau + m_3 \cos 3\tau + \dots, \tag{37}$$

$$(\cos 5\tau - \cos \tau) \cos(A \cos \tau) = \sum_{n=0}^{\infty} n_{2n+1} \cos[(2n+1)\tau] = n_1 \cos \tau + n_3 \cos 3\tau + \dots, \tag{38}$$

$$(\cos 3\tau - \cos \tau) \cos(2A \cos \tau) = \sum_{n=0}^{\infty} f_{2n+1} \cos[(2n+1)\tau] = f_1 \cos \tau + f_3 \cos 3\tau + \dots, \tag{39}$$

and

$$(\cos 5\tau - \cos \tau) \cos(2A \cos \tau) = \sum_{n=0}^{\infty} g_{2n+1} \cos[(2n+1)\tau] = g_1 \cos \tau + g_3 \cos 3\tau + \dots, \tag{40}$$

$$\omega_1 = \frac{b_3 m_1 + b_5 n_1 + \omega_0^2 b_3 + \omega_0^2 b_5 - A b_3 f_1 - A b_5 g_1}{A \omega_0^2}, \tag{41}$$

where  $m_1, n_1, f_1$  and  $g_1$  are given.

Thus, the first-order approximate frequency is

$$\omega = \sqrt{\omega_0^2(1 + \omega_1)}, \tag{42}$$

where  $\omega_0, \omega_1$  are given by equation (23) and (41), respectively, and the corresponding first-order approximate solution is

$$u = (A - b_3 - b_5) \cos \omega t + b_3 \cos 3\omega t + b_5 \cos 5\omega t, \tag{43}$$

where  $b_3, b_5$  are given by equation (34).

#### IV. Results and discussion

We provide a comprehensive analysis of the accuracy and efficiency of the modified homotopy perturbation method (MHPM) across a range of parameters, highlighting its superior performance in frequency and period approximations. Notably, the first-order approximation of frequencies using MHPM delivers exceptionally accurate results for both examples. A critical advancement in this work is the decision to retain the sine function in its entirety rather than employing a Taylor series expansion, as is common in many traditional methods for solving the rotating pendulum equation. While Taylor series expansions are effective for small deflection angles, they introduce significant errors as the pendulum's deflection approaches higher degrees. In contrast, retaining the full sine function allows MHPM to maintain high accuracy, even for large deflection angles.[4]

Detailed comparisons with established methods such as the homotopy analysis method (HAM), gamma function method (GFM), and the coupled method underscore the precision of MHPM. These comparisons, presented in Tables 4.1–4.3, validate the efficacy of the method across various amplitude values. For instance,

in the case of a rotating frame pendulum with  $\Lambda = 0.1$  and  $A = 170^\circ$ , the maximum relative error for the first approximate frequency using MHPM is just 2.35%. In comparison, the Coupled Method and HAM report significantly higher maximum relative errors of 16.97% under the same conditions. Additionally, the GFM demonstrates an even larger relative error of approximately 74.07% for the first approximate frequency at  $\Lambda = 0.1$  and  $A = 160^\circ$ .

Figures 4.2 and 4.2 visually corroborate these findings, illustrating the high accuracy of MHPM for larger amplitudes. The solutions obtained using MHPM closely align with exact solutions, demonstrating the method's robustness and reliability.

Figure 4.2 explores the dual effects of rotational speed ( $\Lambda$ ) and amplitude ( $A$ ) on the rotational pendulum's time period when length  $r$  is constant, revealing two distinct trends: At low rotational speeds  $\Lambda = 0.1$ , the time period increases with amplitude  $A$ , as the rotational speed has minimal influence on pendulum oscillations. Under these conditions, the system behaves similarly to a simple pendulum. At higher rotational speeds  $\Lambda \geq 0.5$ , the rotational speed significantly affects the oscillatory dynamics, leading to a decrease in the time period as  $A$  increases. This behavior highlights the pronounced role of rotational speed in shaping the pendulum's dynamics.[5]

To further evaluate the performance of MHPM, the approximate period are compared to the exact period for the simple pendulum equation, given by

(44)

$$T_{ex} = T_0 \left( 1 + \frac{A^2}{16} + \frac{11A^4}{3072} + \frac{173A^6}{737280} + \frac{22931A^8}{1321205760} + \dots \right),$$

where  $T_0 = 2\pi \sqrt{l/k}$ .

The first approximate period using MHPM is

$$T_{MHPM1} = T_0 \left( 1 + \frac{A^2}{16} + \frac{11A^4}{3072} + \frac{175A^6}{737280} + \frac{23618A^8}{1321205760} + \dots \right), \quad (45)$$

with a limiting value

$$\lim_{A \rightarrow 180} \frac{T_{MHPM1}}{T_{ex}} \cong 1.029952. \quad (46)$$

By contrast, the second approximate period from the harmonic balance method (HBM) is

(47)

$$T_{HBM2} = T_0 \left( 1 + \frac{A^2}{16} + \frac{10A^4}{3072} + \frac{90A^6}{737280} + \dots \right),$$

with a limiting value of

$$\lim_{A \rightarrow 180} \frac{T_{HBM2}}{T_{ex}} \cong 0.520414. \quad (48)$$

Similarly, the second approximate period from the standard homotopy perturbation method (HPM) is

(49)

$$T_{HPM2} = T_0 \left( 1 + \frac{A^2}{16} + \frac{11A^4}{3072} + \frac{173A^6}{737280} + \frac{23898A^8}{1321205760} + \dots \right)$$

with a limiting value of

$$\lim_{A \rightarrow 180} \frac{T_{HMPM2}}{T_{ex}} \cong 1.042150. \quad (50)$$

These comparisons highlight the superior performance of MHPM, which achieves lower relative errors even in its first approximation compared to the higher-order approximations of HBM and HPM.

The results unequivocally demonstrate that MHPM provides a highly accurate and efficient framework for predicting the dynamics of pendulums, particularly under conditions of large deflection angles and for both high and low rotational speeds. By retaining the full sine function and employing a novel approach to approximations, MHPM overcomes the limitations of traditional methods, offering significant advancements in modeling complex nonlinear oscillatory systems.[6]

Table 4.1. Comparison among frequencies obtained various methods for

$$\Lambda = 0.1.$$

$\alpha$	$\omega_e$	$\omega_{HAMI}$ Er(%)	$\omega_{Coupled1}$ Er(%)	$\omega_{HMPM1}$ Er(%)	$\omega_{GMI}$ Er(%)
10°	0.947477	0.947476781 0.0000	0.947476781 0.0000	0.947477 0.0000	0.947475 00.0000
20°	0.943828	0.943830354 0.0002	0.943830354 0.0002	0.943828 0.0000	0.943794 0.0004
30°	0.937654	0.937665034 0.0012	0.937665034 0.0012	0.937654 0.0000	0.937477 0.0189
40°	0.928817	0.928854277 0.0040	0.928854277 0.0040	0.928817 0.0000	0.928254 0.0606
50°	0.917139	0.917234548 0.0104	0.917234548 0.0104	0.917139 0.0000	0.915752 0.1513
60°	0.902406	0.902619454 0.0237	0.902619454 0.0237	0.902406 0.0000	0.899491 0.3230
70°	0.884376	0.884805719 0.0486	0.884805719 0.0486	0.884376 0.0000	0.878884 0.6210
80°	0.862791	0.863595013 0.0932	0.863595013 0.0932	0.862792 0.0001	0.853214 1.1100
90°	0.837376	0.838798882 0.1699	0.838798882 0.1699	0.837379 0.0003	0.8216 1.8840
100°	0.80784	0.810251805 0.2986	0.810251805 0.2986	0.807848 0.0010	0.782916 3.0852
110°	0.773857	0.777818648 0.5119	0.777818648 0.5119	0.773877 0.0026	0.735652 4.9370
120°	0.73504	0.741393859 0.8644	0.741393859 0.8644	0.735092 0.0071	0.677616 7.8124
130°	0.690863	0.700900159 1.4529	0.700900159 1.4529	0.690994 0.0190	0.605291 12.3862
140°	0.640508	0.656274005 2.4615	0.656274005 2.4615	0.640844 0.0525	0.512149 20.0402
150°	0.5825	0.607441391 4.2818	0.607441391 4.2818	0.583403 0.1550	0.382525 34.3305
160°	0.513636	0.554273622 7.9118	0.554273622 7.9118	0.51632 0.5226	0.133175 74.0720
170°	0.424456	0.49650052 16.9735	0.49650052 16.9735	0.434412 1.023458	----- -----

Where Er(%) represents absolute percentage error.

Table 4.2. Comparison among frequencies obtained various methods for

$$\Lambda = 0.5.$$

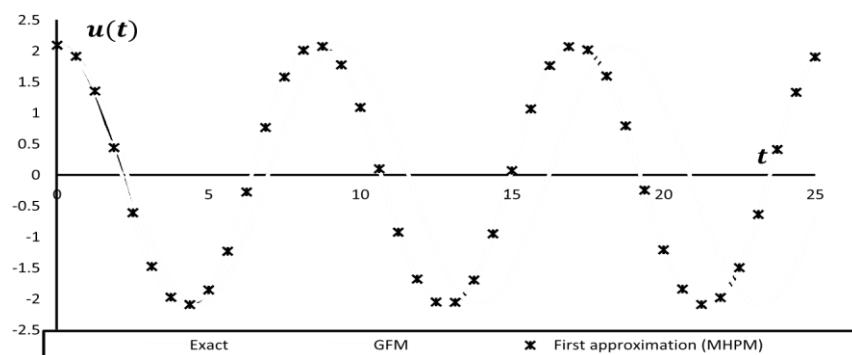
$A$	$\omega_e$	$\omega_{HAMI}$ Er(%)	$\omega_{CoupledI}$ Er(%)	$\omega_{HMPMI}$ Er(%)	$\omega_{GMI}$ Er(%)
10°	0.70977	0.709770265 0.0001	0.709770265 0.0001	0.70977 0.0000	0.709769 0.0000
20°	0.717411	0.717422729 0.0016	0.717422729 0.0016	0.717411 0.0000	0.717396 0.0021
30°	0.729059	0.729107729 0.0067	0.729107729 0.0067	0.729059 0.0000	0.728973 0.0118
40°	0.743283	0.743399142 0.0156	0.743399142 0.0156	0.743283 0.0000	0.742984 0.0403
50°	0.758405	0.758602593 0.0261	0.758602593 0.0261	0.758405 0.0000	0.757608 0.1051
60°	0.772676	0.77293577 0.0336	0.77293577 0.0336	0.772678 0.0002	0.770911 0.2284
70°	0.784415	0.78468068 0.0339	0.78468068 0.0339	0.784417 0.0003	0.780987 0.4370
80°	0.792082	0.792285208 0.0257	0.792285208 0.0257	0.792085 0.0004	0.786044 0.7623
90°	0.79432	0.794422737 0.0129	0.794422737 0.0129	0.794321 0.0001	0.784444 1.2434
100°	0.789963	0.790016374 0.0067	0.790016374 0.0067	0.789959 0.999994	0.774691 1.9333
110°	0.778014	0.778250675 0.0304	0.778250675 0.0304	0.778 0.999982	0.755375 2.9099
120°	0.757597	0.758555771 0.1265	0.758555771 0.1265	0.757579 0.999976	0.706021 6.8079
130°	0.727867	0.730586629 0.3737	0.730586629 0.3737	0.727877 0.0014	0.681997 6.3019
140°	0.687817	0.694187166 0.9262	0.694187166 0.9262	0.687968 0.0220	0.623785 9.3094
150°	0.635859	0.649335149 2.1193	0.649335149 2.1193	0.636513 0.1028	0.546182 14.1033
160°	0.568623	0.596063604 4.8258	0.596063604 4.8258	0.571044 0.4257	0.440009 22.6185
170°	0.475894	0.534319635 12.2770	0.534319635 12.2770	0.485938 2.1106	0.275313 42.1483

Where Er(%) represents absolute percentage error.

Table 4.3. Comparison among frequencies obtained various methods for  $\Lambda = 0.9$ .

A	$\omega_e$	$\omega_{HAMI}$ Er(%)	$\omega_{Coupled}$ Er(%)	$\omega_{HMPM}$ Er(%)	$\omega_{GFM}$ Er(%)
10°	0.331359	0.331414417 0.0166	0.331414417 0.0166	0.331359 0.0000	0.331412 0.0160
20°	0.371673	0.372256865 0.1572	0.372256865 0.1572	0.371674 0.0004	0.372245 0.1540
30°	0.427181	0.428928525 0.4092	0.428928525 0.4092	0.427195 0.0033	0.428885 0.3990
40°	0.489305	0.492459206 0.6447	0.492459206 0.6447	0.48935 0.0093	0.492333 0.6190
50°	0.552065	0.556450032 0.7943	0.556450032 0.7943	0.552157 0.0166	0.556183 0.7460
60°	0.611366	0.61655304 0.8484	0.61655304 0.8484	0.611509 0.0234	0.616055 0.7670
70°	0.664303	0.669750116 0.8199	0.669750116 0.8199	0.664491 0.0283	0.668914 0.6940
80°	0.708738	0.713887975 0.7266	0.713887975 0.7266	0.708955 0.0306	0.712565 0.5400
90°	0.743058	0.747415522 0.5864	0.747415522 0.5864	0.743277 0.0295	0.745436 0.3200
100°	0.766035	0.769248686 0.4195	0.769248686 0.4195	0.766223 0.0245	0.76638 0.0450
110°	0.776727	0.778682523 0.2518	0.778682523 0.2518	0.776841 0.0147	0.774595 0.2744
120°	0.774385	0.775337331 0.1230	0.775337331 0.1230	0.774383 0.999998	0.769562 0.3228
130°	0.758335	0.759113271 0.1026	0.759113271 0.1026	0.758193 0.999813	0.750908 0.9794
140°	0.727766	0.730134472 0.3254	0.730134472 0.3254	0.727526 0.999670	0.718275 1.3042
150°	0.681266	0.688685168 1.0890	0.688685168 1.0890	0.681204 0.999908	0.671047 1.5000
160°	0.61552	0.635109687 3.1826	0.635109687 3.1826	0.6168 0.2079	0.607849 1.2463
170°	0.519821	0.569633982 9.5827	0.569633982 9.5827	0.528323 0.16355	0.525362 1.0660

Where Er(%) represents absolute percentage error.


Figure 4.2. Comparison among the solutions obtained by the modified homotopy perturbation method (MHPM), gamma function method (GFM) with exact solution for  $\Lambda = 0.1$ ,  $A = 120^\circ$ .

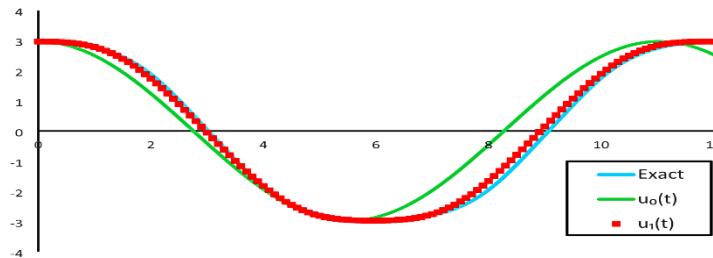


Figure 4.3. Comparison among the zeroth and first-order solutions obtained by the modified homotopy perturbation method (MHPM) with exact solution for  $\Lambda = 0.9$ ,  $A = 170^\circ$ .

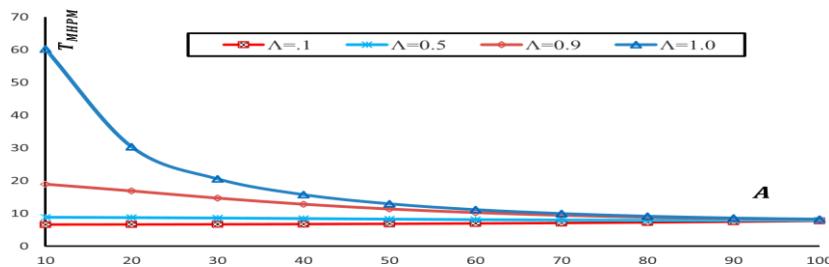


Figure 4.4. Variation of first approximate period obtained by the modified homotopy perturbation method(MHPM) for various values of the parameter  $\Lambda$ .

## V. Conclusion

This paper presents an enhanced application of the Modified Homotopy Perturbation Method (MHPM) to study the nonlinear motion of a rotating pendulum. The method successfully provides high-accuracy estimates for frequency and time period without linearizing the sine function, making it effective even at large amplitudes. Results demonstrate the superiority of MHPM over traditional methods such as HAM, GFM, and HBM in terms of accuracy and convergence speed. The study also highlights the influence of rotational speed and amplitude on the system's behavior, underscoring the value of MHPM in analyzing complex nonlinear dynamical systems.

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