



Research Paper

## An Effect of Different Cutouts shapes of Plate on the Buckling Load of Laminated composites

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### ABSTRACT:

Laminated composite plates consist of layers of bonded materials with varying chemical compositions, assembled in a macroscopic fashion. Plates constructed from laminated composite material with perforations exhibit reduced stiffness, less inertial resistance, and inferior strength compared to solid plates. This study focuses on the optimization and nonlinear behavior of square and cylindrical laminated plates, both with and without cuts, as well as their performance under buckling loads when uncut. Cutouts are needed for several purposes, including ventilation, cable attachments, and weight reduction, and are crucial for achieving the objective of minimizing weight. The assessment procedure considers characteristics such as the cutting position, fiber orientation angle, length-to-thickness ratio, boundary condition, and Young's Modulus Ratio. The examined laminated plates were composed of carbon fiber reinforced composites, which are the materials under investigation. Laminated composite plates with circular cutouts exhibit a reduced buckling load compared to plates without cuts.

**KEYWORDS:** Buckling Load, FEM, Laminated Composite Plate, Cutout shapes.

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### I. INTRODUCTION

Buckling is a characteristic exhibited by composite laminated plates when exposed to compressive forces. Composites consist of two or more materials that, when combined, provide properties that would be challenging to get with a single component alone. The fibers mostly bear the weight of these materials. Matrices with a low modulus and high elongation provide flexible structural performance while protecting fibers from environmental stresses and maintaining their correct alignment. Composite materials, consisting of two or more components, significantly reduce structural weight while maintaining a high strength-to-weight ratio via their composition. In construction, fiber-reinforced composites often manifest as a lamina, which is a slender layer. Laminae are the predominant kind of material macrounit. The stacking sequence of layers and the orientation of fibers in each lamina may be altered to provide the desired strength and stiffness for a particular application. The distinctive features of a composite material arise from the unique mix of traits resulting from the composition, distribution, and orientation of its components. Cutouts are essential for many purposes, including weight reduction, improved air circulation, and the creation of linkages with adjacent components. Carbon-fiber reinforced plastic is a composite material formed by amalgamating several types of carbon fibers with thermosetting resins. Carbon fiber reinforced plastic (CFRP) is an exceptionally durable material that is lightweight, nonconductive, and strengthened with fibers. It is possible to enhance the material's strength and stiffness properties effectively by layering many fiber sheets with various orientations. Parth Bhavsar and colleagues used the finite element approach to examine the buckling behavior of glass fiber reinforced polymer (GFRP) under linearly increasing loads.

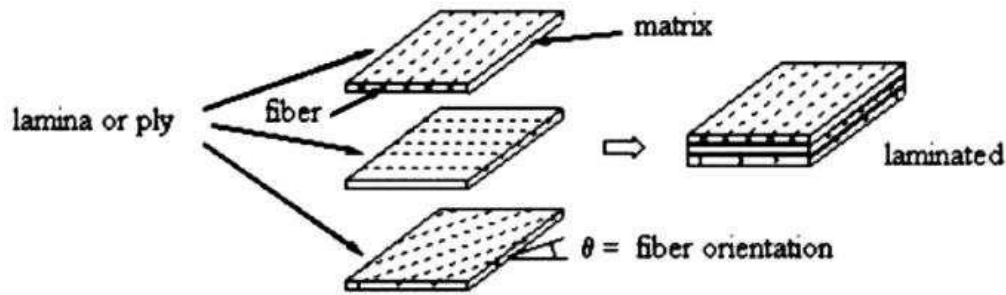


Figure 1: Laminated Composite Plate

Researchers have examined several factors to ascertain their impact on the buckling stress of rectangular plates with an aspect ratio of 1. Joshi et al. used two-dimensional finite element analysis to ascertain the buckling stress per unit length of a rectangular plate with circular cut-outs during bi-axial compression. The buckling factors may be assessed by modifying the length-to-thickness ratio and the placement of the holes. Nagendra Singh Gaira and associates examined the buckling behavior of laminated rectangular plates under clamped-free boundary circumstances. The existence of cut-outs leads to a decrease in the buckling load. As the aspect ratio increases, the buckling load factor decreases, which is the intended outcome. Hamidreza Allahbakhsh and Ali Dadrasi conducted a buckling study on a laminated composite cylindrical panel including an elliptical cut-out of several sizes and positions to examine the effect of an axial load on the panel's buckling load. Container Okutan Baba examines how the buckling stress on rectangular plates is influenced by various cut-out geometries, length-to-thickness ratios, and ply orientations. The researchers used both theoretical and experimental approaches to ascertain the implications of these impacts on the buckling behavior of E-glass/epoxy composite plates subjected to in-plane compression stress. Hsuan-Teh Hu and colleagues, in their finite element buckling analysis of composite laminate skew plates under uniaxial compressive loads, found that the failure criterion and nonlinear in-plane shear significantly influence the ultimate loads of the skew plates, compared to the linearized buckling loads.

### 1. Finite Element Method for Numerical Analysis with Materials

A method that is direct to meet the requirements of the conference paper format This study aims to ascertain the buckling load factors of square and cylindrical carbon fiber composite plates by finite element analysis. The APDL version is ANSYS 14.5. The dimensions of the plate,  $L \times t$ , are analyzed under three distinct boundary conditions: fixed, clamped, and unclamped. The first scenario has two layers, while the second scenario consists of three levels. This is attributable to the used stacking sequences of  $[0^0/90^0]$  and  $[0^0/90^0/0^0]$ , respectively. To conduct the investigation, the plate is perforated with many central holes of identical volume. The center holes may be configured in circular, square, triangular, or star patterns. An inquiry is underway about the characteristics of the buckling load factor.

### 2. Description of Element

This question utilizes the SHELL281 element type. This shell element facilitates the study of shells that are either very thin or comparatively thick. Moreover, because to its stratified uses, it is ideal for modeling sandwich structures and laminated composite coatings. Applications characterized by significant strain nonlinearity, linearity, or rotation are well suited for the use of this material. Each of the eight nodes of the element have six degrees of freedom. These degrees of freedom provide rotation around the three axes and translations along the x, y, and z axes inside the element. Research using cylindrical plates use the nonlinear element S8R5, characterized by eight nodes and five degrees of freedom per node.

### 3. Geometric Modelling

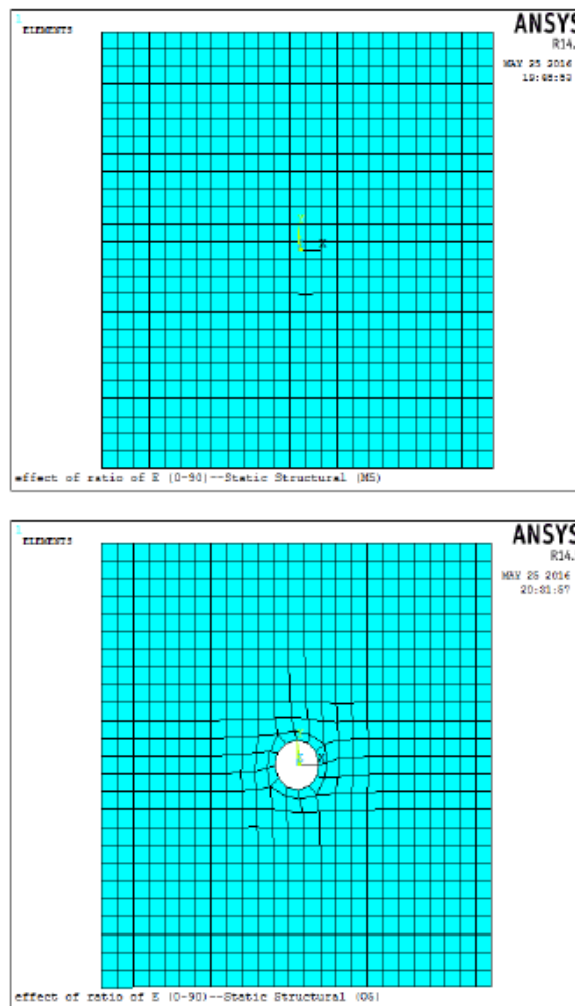
The dimensions of square plates may begin at 500 millimeters. The diameter of the central hole is thought to be fifty millimeters. For cylindrical specimens, nominations may range from L500 to R200. The numeral after the letter L indicates the panel's length, while the numeral following the letter R signifies the panel's radius. The plate is available in four specific thicknesses: 2 millimeters, 2.5 millimeters, 3 millimeters, and 3.5 millimeters.

**Table 1:** Properties of carbon material

Young's modulus (Pa)	$E_{11}=1.397 \times 10^{11}$	$E_{33}=1.139 \times 10^{11}$
Poisson's ratio	$\nu_{12}=0.3236$	$\nu_{13}=0.3236$
Rigidity modulus (Pa)	$G_{12}=4.753 \times 10^9$	$G_{13}=4.753 \times 10^9$

**4. Plate Model of Composite Laminate**

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**Figure 2 :** Model of square plate without and with cut-out

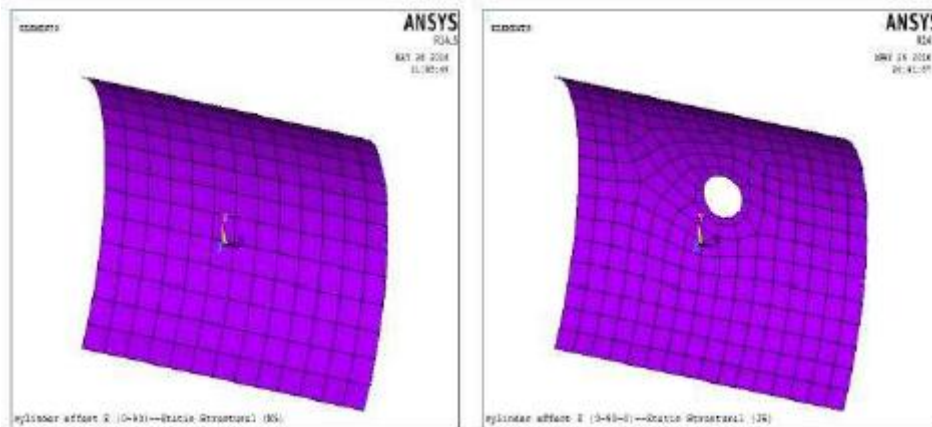


Figure 3: Model of cylindrical plate without and with cut-out

## II. RESULTS AND DISCUSSION

The purpose of this part is to investigate the impact that various ply orientations of the plate have on the plate when it is subjected to the same boundary condition. This will be done at the same time. This specific case is a condition that is fixed at the border, and it is being taken into account. This section makes use of a number of different ply orientations, which are listed below: (0/0/0), (0/30/0), (0/45/0), (0/90/0), (90/90/90), and (90/0/90). Please refer to the following list for further information. Both of them are subjected to analysis, and a study into the repercussions of the situation is carried out.

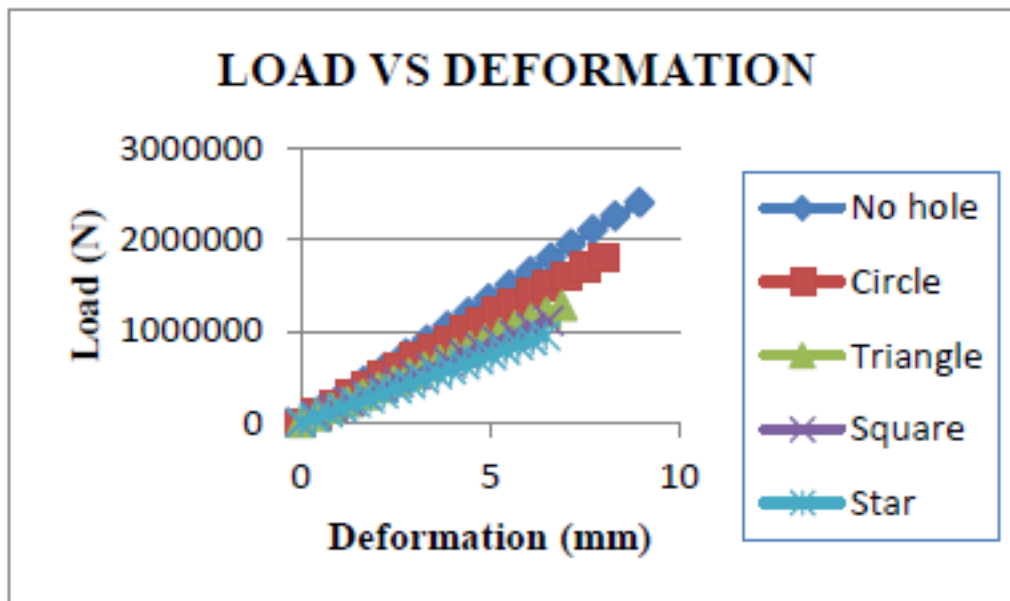


Figure 4 : Buckling load deformation graph of square plate

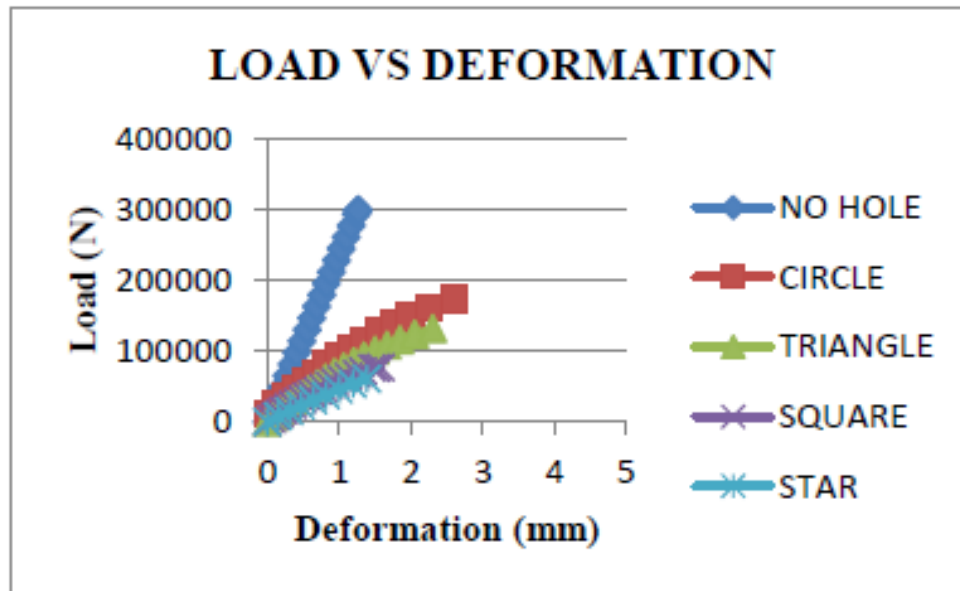


Figure 5 : Buckling load deformation graph of cylindrical plate

Figures 4 and 5 indicate that the buckling load is greater for the plate without a hole. The results demonstrate that the fluctuation of the buckling loads is very sensitive to the existence of cut-outs. The buckling load often diminishes in the presence of a cut-out. The primary objective is to identify the most efficient plate with a cut-out about the buckling load. The findings indicate that the plate with a circular cut-out has a greater capability for bearing buckling loads. The absence of corner points is the reason for the occurrence of stress concentrations. The results demonstrate that the fluctuation of the buckling loads is highly responsive to the existence of cut-outs. The buckling load often diminishes in the presence of a cut-out. Among the triangular, square, and star cutouts, the triangular cutout exhibits a greater buckling load than both the square and star cutouts. The star cut-out exhibits the lowest buckling load-bearing capability due to its greater number of corner points compared to the triangular and square cut-outs. The differences in cut-outs result from changes in stress concentration.

### III. CONCLUSIONS

Buckling response analysis of laminated composite plates with a variety of cutout shapes is being carried out. At the same time, it is of the utmost importance to take into consideration the fact that the laminated composite plates have a variety of aspect ratios, varying width to thickness ratios, cut out shapes, and different placements for holes. In light of the findings of the current investigation, one may draw a wide variety of conclusions, some of which are as follows: There is a correlation between the ratio of the  $L$  to the  $t$  and an increase in the buckling load. The presence of cut-out results in a reduction in the buckling load, which is a consequence of the fact that it is there. There is a reduction in the amount of load that is necessary to buckle the plate and cause it to deform its shape when there is a cut-out present. This is because the surface area lowers when there is a cut-out present. This is due to the fact that the plate is compelled to buckle as a result of the tension. The buckling load is thus decreased as a result of this cause and effect. Buckling load starts to grow in a way that is proportional to the number of layers as the number of layers increases. This occurs as the number of layers increases. Increasing the number of layers results in an increase in the amount of interaction that occurs between each layer. This is the reason why things are the way they are. Consequently, in order to achieve the critical buckling load, a significant amount of load is necessary to be applied to the material. With an increase in the  $EL/ET$  ratio, the buckling load likewise rises in a manner that is proportional to the magnitude of the proportional increase. It is conceivable for the amount of weight that is buckled to alter depending on the cut-out forms that are used. Both of these possibilities are viable. When it comes to circular cut-outs, the buckling load is revealed to be the largest quantity that is even remotely conceivable. Additionally, the buckling load is the lowest value that is capable of being achieved for star cuts of the same size. An extra consideration to take into account is this.

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